Model Reduction for the Spatially Distributed Systems Using the Combined Eigenfunctions and Empirical Eigenfunctions

Mian JIANG*, Yong GUO, Jigang WU, Wenyun WANG

Hunan Provincial Key Laboratory of Health Maintenance for Mechanical Equipment, Hunan University of Science and Technology, XiangTan 411201, China

Abstract: The selection of spatial basis functions will significantly affect the accuracy and efficiency of modeling for nonlinear spatially distributed processes (SDP). The performance using the general spatial basis functions is not good enough which restricts the applications of the approximated models. The current study compares the model reduction performance of empirical eigenfunctions (EEFs) and a kind of new basis functions for the spatially distributed processes, which are obtained from general spatial basis functions by linear transformation, and the transformation matrix is derived using empirical balanced truncation. The EEFs are assumed the optimal in the sense of the least squares errors for the model reduction of spatially distributed processes, however, the results of the simulations show that the accuracy of the modeling based on the present new basis functions is better than that based on the EEFs derived from the measured spatio-temporal data.

Keywords: Spatially Distributed Process; Basis Functions; Empirical Eigenfunctions; Linear Transformation; Empirical Balanced Truncation

1. Introduction

Many of industrial processes such as convection and diffusion reaction process, thermal process and fluid flow belong to SDPs [1]. Their inputs, outputs, states and parameters vary both temporally and spatially. The firstprinciple modeling typically leads to various partial differential equations (PDEs), which such models can accurately predict the nonlinear and spatially distributed dynamical behavior. However, Because of the infinitedimensional nature of these systems, it will does not allow their direct use due to limited computation capacity for numerical implementation and finite actuators/sensors for practical control. Thus, a finite-dimensional modeling is usually required for engineering applications, which makes the model reduction essential to SDP modeling.

The selection of spatial basis functions is important for the accuracy and efficiency of the modeling of nonlinear spatially distributed processes. Under the time–space separation framework[2], different approaches and methods will arise according to the combination proper model reduction approaches and spatial basis functions selection. The popular global basis functions are introduced for model reduction mainly including empirical eigenfunctions (EEFs) [3] and analytical basis functions[4]. However, general analytical basis functions may not be optimal in the sense that the dimension of the reduced model is not the lowest for a given accuracy. Although the model dimension can be further reduced using nonlinear weighted residual method (WRM)[1,5] such as the approximate manifold method[1], the structure of the algorithm is very complex and the computation is significantly large.

As a popular spatial basis functions from the measured data, EEFs are often used for the model reduction of the spatially distributed processes. To obtain the EEFs, a basic assumption is made that the measured data fully represent the temporal progress of a spatially distributed process. Thus, the empirical eigenfunctions also have its limits for the engineering applications. Because the spatio-temporal measured data for the computation of the EEFs depends on the number and locations of the sensors in the spatially distributed processes, the number of the EEFs for the availability of sensors and actuators. Thus, the order and accuracy of the modeling of spatially distributed processes are limited for the only use of the input-output data.

In this note, a kind of new basis functions derived by empirical balanced truncation[6,7,8] is proposed for the modeling of spatially distributed processes. The new spatial basis functions are also obtained by the linear transformation of the general eigenfunctions, and the transformation matrix is derived by empirical balanced truncation for the corresponding high-order nonlinear

HK.NCCP

ordinary differential equation (ODE) systems of SDP s, which is derived using spectral method[9] based on a complete family of eigenfunctions of SDPs. This approach combines the ease of use of linear theory with the flexibility required for modeling of nonlinear spatially distributed processes. The modeling performances of the new basis functions are compared with the empirical eigenfunctions. The results of the simulations show that the accuracy of the modeling based on the present new basis functions is better than that based on the empirical eigenfunctions derived from the measured spatiotemporal data.

2. Eigenfunctions for the Modeling of SDPs

Assume that a nonlinear SDP is governed by a PDE with following state description:

$$\frac{\partial X}{\partial t} = \mathbf{A}X + \mathbf{B}U + F(X, \mathbf{L}, U, \mathbf{L})$$
(1)

In Eq.(1), $t \in [0,\infty)$ is time variable, $z \in \Omega$ is the spatial coordinate, and only one spatial-dimension is considered. A and B are two linear operators that involve linear spatial derivatives for X and U, where X = X(z,t) denotes the vector of state variable and $U = U(z,t) = \sum_{i=1}^{p} u_i(t)h_i(z)$ denotes the vector of spatio-temporal manipulated input. $F(X, \partial X / \partial z, \mathbf{L}, U, \partial U / \partial z, \mathbf{L})$ is a nonlinear function containing spatial derivatives for X(z,t) and U(z,t). Eq.(1) is considered on a bounded spatial domain Ω and subjects to a number of boundary and initial conditions. The phase space of (1) is on the infinitedimensional Hilbert space $H(\Omega)$ of sufficiently smooth functions from Ω into real numbers. A scalar products is introduced in $H(\Omega)$, which is usually given by $[g,h] = \int_{\Omega} g(z)h(z) dz$ for two arbitrary functions $g(z), h(z) \in H(\Omega)$.

A family denotes the infinite set of the eigenfunctions of linear operator \mathbf{A} for PDE (1) is first derived by the following equation:

$$\mathbf{A}\mathbf{f}_{i}(z) = \mathbf{I}_{i}\mathbf{f}_{i}(z), \ i = 1, 2, \mathbf{L}$$
⁽²⁾

This family is a complete family of smooth global spatial orthogonal basis functions $\{f_1(z), f_2(z), \mathbf{L}, \mathbf{L}\}$. The spatio-temporal variable of PDE (1) can be expanded onto the infinite number of eigenfunctions with the corresponding temporal coefficients.

Suppose that the system is controlled by *p* actuators with implemental temporal signal u(t), $u(t) = [u_1(t), u_2(t), \mathbf{L}, u_p(t)]^T$ and certain spatial distributions. The spatiai-temporal output Y(z, t) is measured at M locations. Due to the orthogonal of the eigenfunctions, an infinite-dimensional ODE system can be obtained by the Galerkin method as follows.

To reduce the infinite-dimensional nonlinear ODE system in to a finite set of nonlinear ODE equations, the fast modes are excluded according to the eigenvalues, and the retained finite-dimensional nonlinear ODE system can be rewritten in a general form as follows:

$$\mathbf{\mathscr{K}}(t) = Ax(t) + Bu(t) + f(x(t), u(t))$$

$$y(t) = Cx(t)$$
(3)

 $x(t) = [x_1, x_2, \mathbf{L}, x_N]^T$

Where

$$y(t) = [Y(z_1, t), Y(z_2, t), \mathbf{L}, Y(z_M, t)]^T,$$

$$A = diag(I_1, I_2, \mathbf{L}, I_N),$$

$$B = [b_{ij}]_{N \times p}, b_{ij} = \int_{\Omega} B(h_j(z))f_i(z)dz,$$

$$C = [c_{ij}]_{L \times N}, c_{ij} = j_j(z_i), z_l, l = 1, 2, \mathbf{L}, L \text{ in the } lth$$

of L measured spatial locations.

$$f(x(t),u(t)) = [f_1(x(t),u(t)), f_2(x(t),u(t)), \mathbf{L}, f_N(x(t),u(t))]^T$$

and

$$f_i(\hat{x}(t), u(t)) = \int_{\Omega} F(X, \partial X / \partial z, \mathbf{L}, U, \partial U / \partial z, \mathbf{L}) f_i(z) dz$$

3. New Basis Functions Derived by Balancing of Empirical Gramians

Let each new spatial basis function be a linear combination of the first N eigenfunctions corresponding to finitedimensional nonlinear ODE system (3) of nonlinear spatially distributed processes. Define a basis function transformation matrix S, we have

$$\{j_{1}(z), j_{2}(z), \mathbf{L}, j_{K}(z)\} = \{f_{1}(z), f_{2}(z), \mathbf{L}, f_{N}(z)\} S$$
(4)

where
$$K < N$$
 , $\{f_1(z), f_2(z), L, f_K(z)\}$ and

{ $j_1(z)$, $j_2(z)$, L, $j_N(z)$ } denote new spatial basis functions and eigenfunctions, respectively.

The spatio-temporal variable of the PDE (1) can be expanded onto the new spatial basis functions $f_i(z)$ with

the corresponding temporal coefficients $\overline{x}_i(t)$ as follows.

$$X(z,t) \approx \sum_{i=1}^{K} \overline{x}_{i}(t) f_{i}(z)$$
(5)

Using the basis functions expansions and Galerkin method will transform Eq.(1) into

$$D\mathcal{R}(t) = \overline{Ax}(t) + \overline{Bu}(t) + g(\overline{x}(t), u(t))$$
(6)

Let the D^{-1} denotes the inverse matrix of D, S_i denotes

the i th column of the matrix S then a nonlinear ODE system with fewer modes of nonlinear PDE (1) can be derived as follows.

HK.NCCP

International Journal of Intelligent Information and Management Science ISSN: 2307-0692 Volume 3, Issue 4, August 2014

$$D_{ij} = \int_{\Omega} f_i(z) f_j(z) dz = \sum_{k=1}^{N} S_{ki} S_{kj} \int_{\Omega} j_i(z) j_j(z) dz = S_i^T S_j$$

$$\bar{A}_{ij} = \int_{\Omega} \mathbf{A}(f_j(z)) f_i(z) dz = \int_{\Omega} \mathbf{A}\left(\sum_{k=1}^{N} S_{kj} j_k(z)\right) \sum_{k=1}^{N} S_{kj} j_k(z) dz = S_i^T A S_j$$

$$\bar{B}_{ij} = \int_{\Omega} \mathbf{B}(h_j(z)) f_i(z) dz = \int_{\Omega} \mathbf{B}(h_j(z)) \left(\sum_{k=1}^{N} S_{kj} j_k(z)\right) dz = S_i^T B_j$$

$$\bar{C}_{ij} = f_j(z_i) = \begin{bmatrix} c_{i1} & c_{i2} & \mathbf{L} & c_{iN} \end{bmatrix} S_j,$$

$$=\int_{\Omega}F\left(\sum_{i=1}^{K}\overline{x_{i}}(t)f_{i}(z),\frac{\partial\left(\sum_{i=1}^{K}\overline{x_{i}}(t)f_{i}(z)\right)}{\partial z},\mathbf{L},\sum_{i=1}^{p}u_{i}(t)h_{i}(z),\frac{\partial\left(\sum_{i=1}^{p}u_{i}(t)h_{i}(z)\right)}{\partial z},\mathbf{L}\right)f_{j}(z)dz$$

In this section, an algorithm to obtain the spatial basis functions transformation matrix by empirical balanced truncation[6-8] is present for the nonlinear ODE system (3), taking explicit account of the input-output connection of the system. For the nonlinear system (3), the following sets need to be defined for empirical gramians. Let $T^N = \{T_1, T_2, \mathbf{L}, T_r\}$ be a set of r orthogonal $N \times N$ matrices, where r denotes the number of matrices for excitation/perturbation directions. Let $M^{s} = \{c_{1}, c_{2}, \mathbf{L}, c_{s}\}$ be a set of s positive constants, where s denotes the number of different excitation/perturbation sizes for each direction. Let $E^{p} = \{e_{1}, e_{2}, \mathbf{L}, e_{n}\}$ be p standard unit vectors in \mathfrak{R}^{p} , where p denotes the number of inputs to the system (3). Given a function x(t), define the mean by $\langle x(t) \rangle = \lim_{T \to \infty} \int_0^T x(t) dt / T$. For system (3), define the empirical controllability gramian by

$$\hat{W}_{C} = \sum_{l=1}^{r} \sum_{m=1}^{s} \sum_{i=1}^{p} \frac{1}{rsc_{m}^{2}} \int_{0}^{\infty} \Phi^{ilm}(t) dt$$
(8)

Where Φ^{i}

$$\Phi^{ilm}(t) \in \Re$$
 is given

by

 $\Phi^{ilm}(t) = (x^{ilm}(t) - \overline{x}^{ilm})(x^{ilm}(t) - \overline{x}^{ilm})^T$, and $x^{ilm}(t)$ is the state of system(3) corresponding to the impulsive input $u(t) = c_m T_i e_i d(t)$.

For system (3), define the empirical observability gramian by

$$\hat{W}_{o} = \sum_{l=1}^{r} \sum_{m=1}^{s} \frac{1}{rsc_{m}^{2}} \int_{0}^{\infty} T_{l} \Psi^{lm}(t) T_{l}^{T} dt$$
(9)

Where $\Psi^{ilm}(t) \in \Re^{N \times N}$ is given by

$$\Psi_{ij}^{lm}(t) = (y^{ilm}(t) - \overline{y}^{ilm})^T (y^{ilm}(t) - \overline{y}^{ilm}), \text{ and } y^{ilm}(t)$$

is the output of system(3) corresponding to the initial condition $x_0 = c_m T_i e_i$ with the u(t) = 0.

The empirical controllability gramian and empirical observability gramian are computable generalization of controllability gramian and observability gramian to nonlinear systems. It therefore led to a methodology for model reduction of nonlinear ODE system (3) motivated by a standard idea from realization theory. Because the empirical gramians are by the nature based upon discrete measured of system properties, like states and outputs, it is advantageous to reformulate them in a discrete form for numerically calculation. A simple numerical technique for balancing the empirical gramians \hat{W}_c and \hat{W}_o is shown as follows. First, apply the Cholesky factorization[10] to \hat{W}_o so that $\hat{W}_o = ZZ^T$, where Z is a lower triangular matrix with non-negative diagonal entries. Let $U\Sigma^2 U^T$ be a eigenvalue decomposition of $Z^T \hat{W} c Z$. Thus, $\overline{S} = \Sigma^{1/2} U^T Z^{-1}$, and the transformed empirical gramians $\overline{W}_{c} = \overline{S}\hat{W}_{c}\overline{S}^{T}; \quad \overline{W}_{o} = (\overline{S}^{-1})^{T}\hat{W}_{o}\overline{S}^{-1}.$

The nonlinear ODE system (3) that is balanced has the following form, which empirical controllability gramian \overline{Wc} and empirical observability gramian \overline{Wo} are equal to $\Sigma = diag(s_1, s_2, \mathbf{L}, s_N)$. $s_1 \ge s_2 \ge s_3 \ge \mathbf{L} s_N \ge 0$ and the s_i 's are the Hankel singular values. The columns of \overline{S} may be thought of as giving the modes of the system associated with the Hankel singular values in Σ . To derive a superior set of new spatial basis functions, the first K columns of matrix \overline{S} of balancing of the empirical gramians is selected to be a $N \times K$ spatial basis functions transformation matrix. Using the MATLAB style colon notation, transformation matrix $S = \overline{S}(:,1:K)$. The performance of the new spatial

International Journal of Intelligent Information and Management Science ISSN: 2307-0692 Volume 3, Issue 4, August 2014

basis functions from this transformation matrix is illustrated by a numerical example.

4. Comparisons of the Performance with Empirical Eigenfunctions

In order to compare the modeling performance with empirical eigenfunctions for nonlinear spatially distributed processes, a long thin rod[11] in a reactor as is studied which is a typical transport-reaction process in the chemical industry. The reactor is fed with pure species A and a zeroth order exothermic catalytic reaction of the form $A \rightarrow B$ takes place in the rod. Since the reaction is exothermic, a cooling medium that is in contact with the road is used for cooling.

After choosing spatial orthogonal basis functions for time/space separation, the set of new spatial basis functions and empirical eigenfunctions are used for modeling of the nonlinear spatially distributed processes respectively.

Suppose that Y(z,t) and $\overline{Y}(z,t)$ are the measured output and the prediction output at M spatial locations $z_1, z_2, \mathbf{L}, z_M$ and some sampling times $t_1, t_2, \mathbf{L}, t_{Niim}$, respectively. The root of mean square error (RMSE) between the real dynamical process and the approximation model is defined as the performance index as follows:

$$RSME = \sqrt{\sum_{i=1}^{M} \sum_{j=1}^{Nim} \left(Y\left(z_{i}, t_{j}\right) - \hat{Y}\left(z_{i}, t_{j}\right) \right)^{2} / M \cdot Ntim}$$
(10)

Under the assumption of constant density and heat capacity of the rod, constant conductivity of the rod, and constant temperature at both sides of the rod, and excess of species A in the furnace, the mathematical model that describes the spatio-temporal evolution of the rod temperature consists of the following parabolic PDE:

$$\frac{\partial X(z,t)}{\partial t} = \frac{\partial^2 X(z,t)}{\partial z^2} + b_T \left(e^{-g/(1+T)} - e^{-g} \right) + b_u \left(h(z)^T u(t) - X(z,t) \right)$$
(11)

In this study, (11) subject to the following Dirichlet boundary and initial conditions:

$$X(0,t) = 0, X(p,t) = 0, X(z,0) = X_0(z)$$
 (12)

Where X(z,t), u(t), h(z), b_T , b_u , g denote the temperature in the reactor, the manipulated input (temperature of the cooling medium), the actuator distribution, the heat of reaction, the heat transfer coefficient, and the activation energy, respectively. The process parameters are set to be $b_T = 50$, $b_u = 2$, g = 4. There are four actuators $u(t) = [u_1(t), u_2(t), \mathbf{L} u_4(t)]^T$ available with the spatial distribution functions $h(z) = [h_1(z), h_2(z), \mathbf{L} h_4(z)]^T$, where $h_i(z) = H(z - (i - 1)p/4) - H(z - ip/4)$, i = 1, 2, 3, 4 and $H(\cdot)$ is the standard Heaviside function. The input signals are selected as $u_i(t) = 1.1 + 4\sin(t/10 + i/10), i = 1, 2, 3, 4$. Suppose that nineteen sensors uniformly distributed in the space are used for measurement. Four hundred data for each sensor location is collected from (11). The sampling interval Δt is 0.01s and the simulation time is 4s. The initial condition $X_0(z)$ is set to be $\sin(z)$.

To compare the modeling performance based on the new basis functions and EEFs with the same order, the same input signals are used. Nineteen sensors that have been uniformly distributed in the space are used for measurements. The random process noise is bounded by 0.3 with zero mean. The EEFs used for time/space separation and dimension reduction are selected from Karhunen-Loeve (KL) decomposition. In the Galerkin method, obtaining an exact analytical description of the low-dimensional ODE systems is difficult because of the nonlinearities in the system. Therefore, the neural networks are used to identify the long-term dynamics from the inputs and temporal coefficients. As the energy percentage of the first three EEFs has reached larger than 99%, the RMSEs of the approximated models based on two kinds of basis functions on testing data are compared in Table S1 in support information. As shown in Table 1, the values of the RMSE using the new spatial basis functions are little smaller than when using the same number of EEFs.

Table 1.	Comparisons	for	RMSEs	with	empirical
		c .	- 4 *		

eigenfunctions						
RMSE	K = 1	K = 2	K = 3			
EEFs	0.3023	0.1987	0.0930			
New spatial basis functions	0.2879	0.1652	0.0822			

From the Table 1, the RMSEs for the predicted temperature distributions of approximate models based on the proposed new spatial basis functions of kind two and EEFs are 0.0822 and 0.0930, respectively. In many cases, EEFs are frequently used in Galerkin projections to obtain low-dimensional models of DPSs. However, the optimality of the KL decomposition lies in a posteriori data reconstruction, and there are no guarantees of optimality in modeling. In order to illustrate the details of the comparisons for the two kinds of spatial basis functions, the first three EEFs and the first new spatial basis functions are shown in Figure 1 and Figure 2 respectively.



Figure 1. The first three empirical eigenfunctions



Figure 2. The first three new spatial basis functions



Figure 3. Temperature distributions with a three-order approximate model based on new basis functions



Figure 4. Temperature distributions with a three-order approximate model based on empirical eigenfunctions

The approximate temperature distributions of the catalytic rod based on a three-order dynamical model and a three-order dynamical model based on EEFs are shown in Figure 3 and 4, respectively. Apparently, the performance of temperature distribution with a three-order approximate model based on new basis functions in Figure 3 is better than that based on three EEFs in Figure 4.

Conclusion

The current study compares the model reduction performance of empirical eigenfunctions (EEFs) and a kind of new basis functions for the spatially distributed processes, which are obtained from general spatial basis functions by linear transformation, and the transformation matrix is derived using empirical balanced truncation. The proposed new basis functions were calculated using the linear theory of matrix computation for nonlinear processes. The results of the simulations showed that the accuracy of the modeling based on the present new basis functions was better than that based on the empirical eigenfunctions derived from the measured spatio-temporal data.

Acknowledgment

This project is supported by National Natural Science Foundation of China (Grant No. 51305133). Open Fund of State Key Laboratory of Mechanical System and Vibration (MSV201404), Financial Support from National Natural Science Foundation of Hunan province (13JJB007), Project of The Education Department of Hunan Province (13C317,12C0117), Open Fund of Hunan Provincial Key Laboratory of Health Maintenance for Mechanical Equipment are also gratefully acknowledged.

References

- [1] Christofides, P.D. Nonlinear and robust control of PDE systems: Methods and applications to transport-reaction processes; Birkhauser: Boston, MA, 2001.
- [2] Li, H. X.; Qi, C. K. Modeling of distributed parameter systems for applications—A synthesized review from time-space separation. J. Process Control 2010, 20(8), 891.
- [3] Park, H. M.; Cho, D. H. The use of the Karhunen-Loeve decomposition for the modeling of distributed parameter systems. Chem. Eng. Sci. 1996, 51, 81.
- [4] Baker, J.; Christofides P. D. Finite-dimensional approximation and control of non-linear parabolic PDE systems. Int. J. Control 2000, 73(5), 439.
- [5] Ray, W.H. Advanced process control; Butterworths: NewYork, 1981.
- [6] Lall A.; Marsden J. E. ; Glavaski S. A subspace approach to balanced truncation for model reduction of nonlinear control system. Inter. J. Robust and Nonlin. Control 2002, 12, 519.
- [7] Hahn, J.; Edgar T.F. An improved method for nonlinear model reduction using balancing of empirical gramians. Comput. Chem. Eng. 2002, 26(10), 1379.
- [8] Hahn, J.; Edgar, T.F. Balancing approach to minimal realization and model reduction of stable nonlinear systems. Ind. Eng. Chem. Res. 2002, 41(9), 2204.
- [9] Boyd J.P. Chebyshev and Fourier Spectral Methods; Dover Publications: NewYork, 2001.

HK.NCCP

International Journal of Intelligent Information and Management Science ISSN: 2307-0692 Volume 3, Issue 4, August 2014

[10] Golub G. H.; CF V. L., eds. Matrix Computations. Johns Hopkins University Press: Washington, D.C., 1996. parameter processes. Computers & Chemical Engineering, 2009. 33(7): 1247-1260.

[11] Qi, C.K. and Li H.X., A time/space separation-based Hammerstein modeling approach for nonlinear distributed